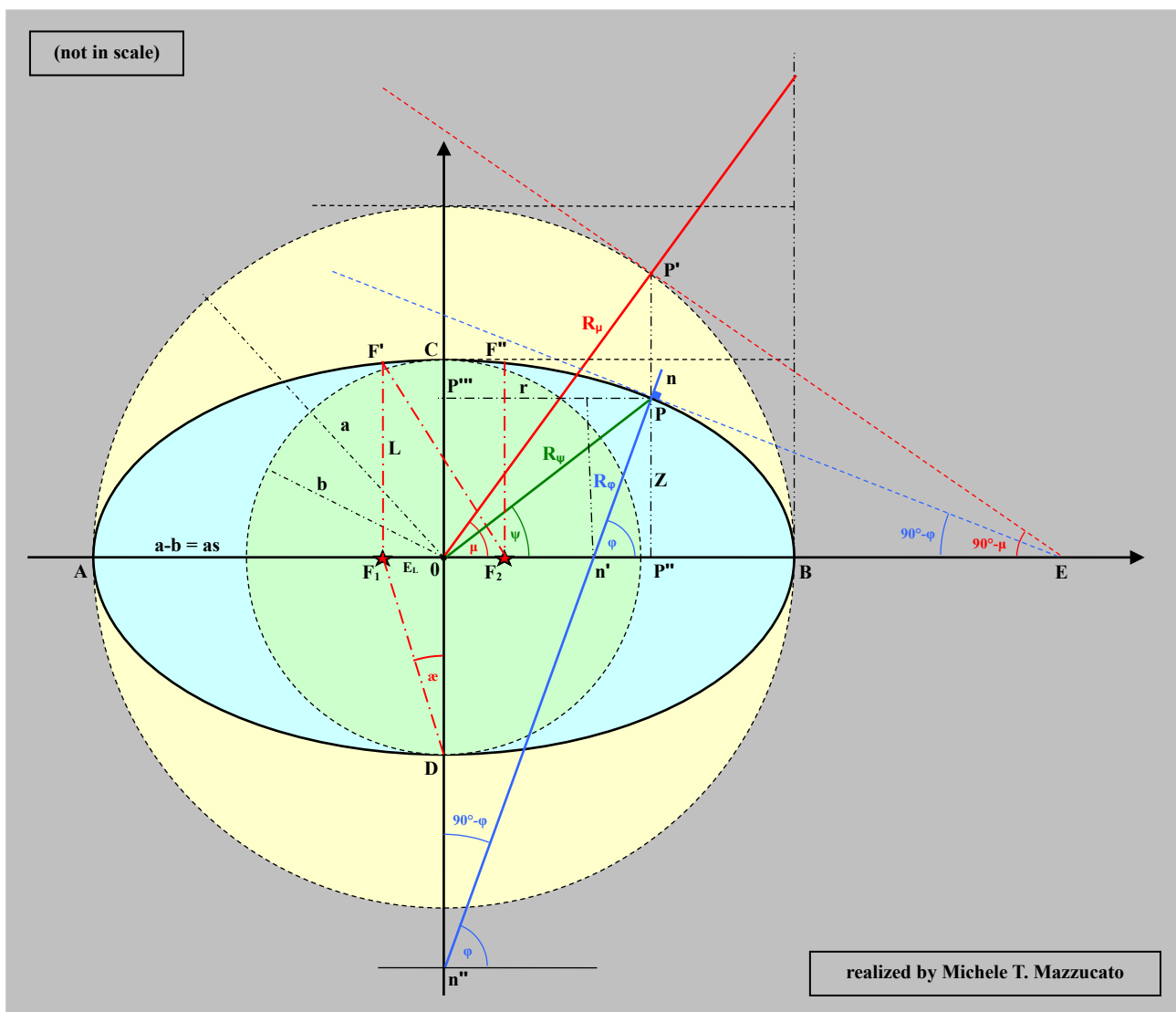


Geometrical relations on Meridian Section



known data	derived data
a equatoriale radius (6378388,000 m) [6378137,000 m]	$e^2 = \frac{a^2 - b^2}{a^2}$ first eccentricity (0,006722670022) [0,006739496743]
b polar radius (6367911,946 m) [6356752,314 m]	$s = \frac{a - b}{a}$ flattening (0,003367003367) [0,003352810665]
a equatoriale radius (6378388,000 m) [6378137,000 m]	$e^2 = 2s - s^2$ first eccentricity (0,006722670022) [0,006739496743]
s flattening (0,003367003367) [0,003352810665]	$b = a(1 - s) = a\sqrt{1 - e^2}$ polar radius (6367911,946 m) [6356752,314 m]

(values IRE24) [values WGS84]

Note: relations between e, e', s and E_L

$$(1-s)^2 = (1-e^2) \quad 1-s = \sqrt{1-e^2} = \frac{b}{a} = \frac{e}{e'} \quad (1-e^2)(1+e'^2) = 1 \quad 1/s = \frac{e'}{e'-e} \quad e = \frac{E_L}{a}$$

$$e^2 = \frac{e'^2}{1+e'^2} = \frac{a^2-b^2}{a^2} \quad e'^2 = \frac{e^2}{1-e^2} = \frac{a^2-b^2}{b^2}$$

Note: canonical (or normal) equation of the ellipse in cartesian coordinates

$$\frac{X^2}{a^2} + \frac{Z^2}{b^2} = 1 \quad \text{and} \quad b^2X^2 + a^2Z^2 = a^2b^2 \quad \text{equation in not canonical form}$$

and in polar coordinates

$$r_{\theta 1} = \frac{a(1-e^2)}{1-e \cos \theta} = \frac{L}{1-e \cos \theta} \quad \text{origin on focus } F_1 \quad \text{and} \quad r_{\theta 2} = \frac{a(1-e^2)}{1+e \cos \theta} = \frac{L}{1+e \cos \theta} \quad \text{origin on focus } F_2$$

$$\overline{F_1 F'} + \overline{F_2 F'} = 2a = \text{constant}$$

equatorial radius (raggio equatoriale)

$$a = \overline{OP''} + \overline{P''B} = \overline{F_1 C} = \overline{F_1 D} = \overline{F_2 C} = \overline{F_2 D} = \overline{OA} = \overline{OB}$$

(6 378 388,000 m)
[6 378 137,000 m]

polar radius (raggio polare)

$$b = \overline{OC} = \overline{OD} = \overline{On'} + \overline{n'P''} + \overline{P''O'}$$

(6 356 911,946 m)
[6 356 752,314 m]

radius of curvature in the prime vertical (raggio di curvatura in primo verticale - gran normale)

$$\overline{n''P} = N = \frac{a}{\sqrt{1-e^2 \sin^2 \varphi}} = \frac{r}{\cos \varphi} = N(1-e^2) + Ne^2 = R_\varphi + Ne^2$$

(6 382 220,751 m)
[6 381 953,457 m]

3D cartesian coordinate (coordinate cartesiane 3D)

$$X = \overline{OP''} = N \cos \varphi \cos \lambda$$

(5 784 256,365 m)
[5 784 014,115 m]

$$Y = N \cos \varphi \sin \lambda$$

(0,000 m)
[0,000 m]

$$Z = \overline{PP''} = R_\psi \sin \varphi = N(1-e^2) \sin \varphi$$

(2 679 110,365 m)
[2 679 074,463 m]

latitude and colatitude ellipsoidal (latitudine e colatitudine ellissoidica)

$$\tan \varphi = \frac{a^2}{b^2} \tan \psi = \frac{a}{b} \tan \mu = \frac{a^2 Z}{b^2 r} = \frac{Z}{r(1-e^2)} = \frac{Z}{N(1-e^2) \cos \varphi}$$

$$\chi_\varphi = 90^\circ - \varphi$$

(25°)
(65°)
[25°]
[65°]

latitude and colatitude ellipsocentric (latitudine e colatitudine ellissocentrica)

$$\tan \psi = \frac{\overline{n'P} \sin(180^\circ - \varphi)}{\overline{On'} - \overline{n'P} \cos(180^\circ - \varphi)} =$$

$$= \frac{N(1-e^2) \sin(180^\circ - \varphi)}{Ne^2 \cos \varphi - N(1-e^2) \cos(180^\circ - \varphi)}$$

Law of Cosines

$$\tan \psi = \frac{Z}{X} = \frac{b^2}{a^2} \tan \varphi = \frac{b}{a} \tan \mu \quad \chi_\psi = 90^\circ - \psi$$

(24,852290°)
(65,147710°)
[24,852913°]
[65,147087°]

Note: $\cos^2 \psi + \sin^2 \psi = 1$

latitude and colatitude parametric (latitudine e colatitudine parametrica)

$$\tan \mu = \sqrt{1 - e^2} \tan \varphi = \frac{a}{b} \tan \psi$$

$$\chi_{\mu} = 90^\circ - \mu$$

(24,926065°)
(65,073935°)
[24,926377°]
[65,073623°]

Note on latitudes: in absolute value $\Psi < \mu < \varphi$, except at the poles and at the equator where they coincide.

parallel radius (raggio del parallelo)

$$\overline{PP'''} = r = \frac{a}{\sqrt{1 - e^2 \sin^2 \varphi}} \cos \varphi = N \cos \varphi = a \cos \mu = R_{\psi} \cos \psi$$

(5 784 256,365 m)
[5 784 014,115 m]

ellipsoidal radius (raggio ellissoidico)

$$\overline{n'P} = R_{\varphi} = N(1 - e^2) = \frac{Z}{\sin \varphi}$$

(6 339 315,187 m)
[6 339 230,236 m]

ellipsocentric radius (raggio ellissocentrico)

$$\overline{OP} = R_{\psi} = N \cos \varphi \sqrt{1 + (1 - e^2) \tan^2 \varphi} = \frac{\sqrt{1 - e^2} (2 - e^2) \sin^2 \varphi}{\sqrt{1 - e^2 \sin^2 \varphi}} = \sqrt{\overline{OP''} + \overline{PP''}} = \sqrt{X^2 + Z^2}$$

$$\overline{OP} = R_{\psi} = R_{\psi}^2 + (Ne^2 \cos \varphi)^2 - 2R_{\varphi} (Ne^2 \cos \varphi) \cos(180^\circ - \varphi) =$$

$$= [N(1 - e^2)]^2 + (Ne^2 \cos \varphi)^2 - 2N(1 - e^2)(Ne^2 \cos \varphi) \cos(180^\circ - \varphi)$$

Law of Cosines

$$\overline{OP} = R_{\psi} = \frac{ab}{\sqrt{(b \cos \psi)^2 + (a \sin \psi)^2}} = \frac{b}{\sqrt{1 - (e \cos \psi)^2}}$$

(6 374 578,734 m)
[6 374 343,830 m]

Note:

$Z = mX$ equation of the straight line passing through the origin of the ellipse with $m = \tan \psi$ slope of the straight line

$b^2 X^2 + a^2 Z^2 = a^2 b^2$ equation in not canonical form of the ellipse

$$b^2 X^2 + a^2 (mX)^2 - a^2 b^2 = b^2 X^2 + a^2 m^2 X^2 - a^2 b^2 = 0$$

$$X = \sqrt{\frac{a^2 b^2}{b^2 + a^2 m^2}} \quad \text{and} \quad Z = mX \quad R_{\psi} = \sqrt{X^2 + Z^2}$$

parametric radius (raggio parametrico)

$$\overline{OP'} = R_{\mu} = a$$

(6 378 388,000 m)
[6 378 137,000 m]

angular eccentricity (eccentricità angolare)

$$\alpha = \arccos \frac{b}{a} = 2 \arctan \sqrt{\frac{a - b}{a + b}} = \arcsen e$$

(4,703069°)
[4,693141°]

linear eccentricity (eccentricità lineare)

$\overline{OF_1} = \overline{OF_2} = E_L = \sqrt{a^2 - b^2} = ae = a \sin \alpha$	(522 976,087 m) [521 854,008 m]
$\overline{PP''} = Z = \sqrt{n'P^2 - \overline{OP''}^2} = R_\varphi \sin \varphi = \sqrt{\overline{OP}^2 - \overline{OP''}^2} = R_\psi \sin \psi = b \sin \mu$	(2 679 110,365 m) [2 679 074,463 m]
$\overline{P'P''} = \sqrt{\overline{OP'}^2 - \overline{OP''}^2} = \sqrt{a^2 - X^2} = a \sin \mu$	(2 688 161,413 m) [2 688 087,110 m]
$\overline{PP'} = \overline{P'P''} - \overline{PP''} = \sqrt{a^2 - X^2} - Z$	(9 051,049 m) [9 012,647 m]
$\overline{n'n''} = \overline{n''P} - \overline{n'P} = N - R_\varphi = Ne^2$	(42 905,564 m) [42 723,222 m]
$\overline{P''B} = \overline{OB} - \overline{OP''} = a - r$	(594 131,635 m) [594 122,885 m]
$\overline{OP''} = Ne^2 \cos \varphi + N(1 - e^2) \cos \varphi = a \cos \mu$	(5 784 256,365 m) [5 784 014,115 m]
$\overline{n'P''} = R_\varphi \cos \varphi = N(1 - e^2) \cos \varphi$	(5 745 370,718 m) [5 745 293,726 m]
$\overline{On'} = \overline{OP''} - \overline{n'P''} = Ne^2 \cos \varphi$	(38 885,647 m) [38 720,388 m]
$\overline{P''O'} = \overline{OO'} - \overline{OP''} = b - r$	(572 655,581 m) [572 738,200 m]
$\overline{On''} = Ne^2 \sin \varphi$	(18 132,675 m) [18 055,614 m]
$\overline{P'''n''} = N \sin \varphi$	(2 697 243,040 m) [2 697 130,077 m]
$\overline{PE} = \frac{\overline{PP''}}{\sin(90^\circ - \varphi)} = \frac{\overline{PP''}}{\sin \chi_\varphi} = \frac{\overline{PP''}}{\cos \varphi} = \overline{n'E} \sin \varphi$	(2 956 071,219 m) [2 956 031,606 m]
$\overline{P'E} = \frac{\overline{P'P''}}{\sin(90^\circ - \mu)} = \frac{\overline{P'P''}}{\sin \chi_\mu} = \frac{\overline{P'P''}}{\cos \mu} = \overline{OE} \sin \mu = a \tan \mu$	(2 964 276,723 m) [2 964 202,285 m]
$\overline{P''E} = \overline{P'P''} \tan \mu = \overline{P'E} \sin \mu = \overline{P'E} \cos \chi_\mu = \overline{OE} - r = \overline{PE} \tan \varphi = \overline{PE} \sin \varphi = \overline{PE} \cos$	(1 249 289,680 m) [1 249 272,939 m]
$\overline{n'E} = \frac{R_\varphi}{\cos \varphi}$	(6 994 660,398 m) [6 994 566,665 m]

$\overline{OE} = \frac{a}{\cos \mu}$	(7 033 546,045 m) [7 033 287,054 m]
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focal distance (distanza focale)

$\overline{F_1F_2} = 2E_L = 2\sqrt{a^2 - b^2}$	(1 045 952,174 m) [1 043 708,017 m]
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straight semilated (semilato retto)

$\overline{F_1F'} = \overline{F_2F''} = L = \frac{b^2}{a} = a(1 - e^2)$	(6 335 508,202 m) [6 335 439,327 m]
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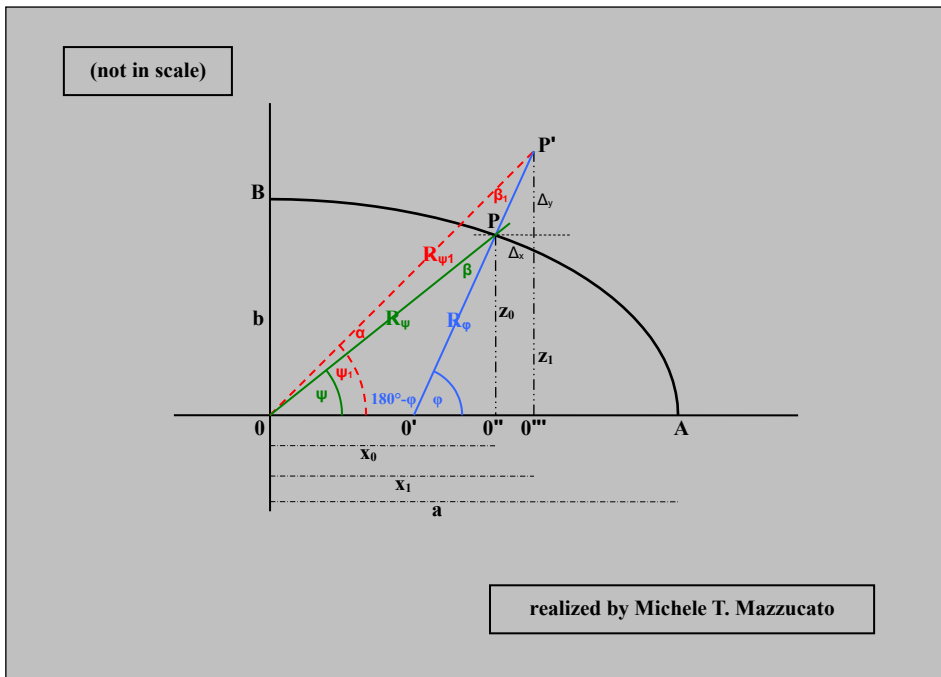
equatorial diameter (diametro equatoriale)

$\overline{AB} = \overline{F_1F'} + \overline{F_2F'} = 2a$	(12 756 776,000 m) [12 756 274,000 m]
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polar diameter (diametro polare)

$\overline{CD} = 2b$	(12 713 823,892 m) [12 713 504,628 m]
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$\overline{F_2F'} = \sqrt{\overline{F_1F'}^2 + 2E_L^2}$	(6 421 267,798 m) [6 420 834,673 m]
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$\overline{OO''} = X_0 = \overline{OO'} + \overline{O'O''} = N \cos \varphi$	(5 784 256,365 m) [5 784 014,115 m]
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$\overline{OO''' } = X_1 = \overline{OO'} + \overline{O'O''} + \overline{O''O'''} = (N + h) \cos \varphi$	(5 784 703,175 m) [5 784 460,924 m]
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$\Delta_x = \overline{O''O'''} = \overline{O''A} - \overline{O'''A} = X_1 - X_0$	(446,810 m) [446,809 m]
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$\overline{O''A} = a - X_0$	(594 131,635 m) [594 122,885 m]
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$\overline{O''A} = a - X_1$	(593 684,825 m) [593 676,076 m]
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$\overline{O'O''} = N(1 - e^2) \cos \varphi$	(5 745 370,718 m) [5 745 293,727 m]
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$\overline{OO'} = \overline{OO''} - \overline{O'O''} = X_0 - \overline{O'O''} = N \cos \varphi - N(1 - e^2) \cos \varphi = Ne^2 \cos \varphi$	(38 885,647 m) [38 720,388 m]
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$\overline{PO''} = Z_0 = N(1 - e^2) \sin \varphi$	(2 679 110,365 m) [2 679 074,463 m]
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$\overline{PO'''} = Z_1 = [N(1 - e^2) + h] \sin \varphi$	(2 679 318,716 m) [2 679 282,814 m]
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$\Delta_y = Z_1 - Z_0$	(208,351 m) [208,351 m]
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$\overline{O'P} = R_\varphi = N(1 - e^2)$	(6 339 315,187 m) [6 339 230,236 m]
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$\overline{OP} = R_\psi = \sqrt{X_0^2 + Z_0^2}$ $\overline{OP} = R_\psi = \sqrt{\overline{OO''}^2 + \overline{O'P}^2 - 2 \overline{OO''} \overline{O'P} \cos(180^\circ - \varphi)} =$ $= \sqrt{[Ne^2 \cos \varphi]^2 + [N(1 - e^2)]^2 - 2[Ne^2 \cos \varphi][N(1 - e^2)] \cos(180^\circ - \varphi)} \quad \text{Law of Cosines}$ $\overline{OP} = R_\psi = \frac{\overline{O'P} \sin(180^\circ - \varphi)}{\sin \psi} = \frac{\overline{OO''} \sin(180^\circ - \varphi)}{\sin \beta} \quad \text{Law of Sines}$	(6 374 578,734 m) [6 374 343,830 m]
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Note: spherical coordinates

$$X = R_\psi \cos \psi \cos \lambda$$

$$Y = R_\psi \cos \psi \sin \lambda$$

$$Z = R_\psi \sin \psi$$

$$R_\psi = \sqrt{X^2 + Y^2 + Z^2} \quad R_\psi = \frac{Z}{\sin \psi} = \frac{Y}{\cos \psi \sin \lambda} = \frac{X}{\cos \psi \cos \lambda} \quad R_\psi = \frac{\sqrt{X^2 + Y^2}}{\cos \psi}$$

$$\tan \psi = \frac{Z}{\sqrt{X^2 + Y^2}} \quad \cos \psi = \frac{\sqrt{X^2 + Y^2}}{R_\psi} \quad \tan \lambda = \frac{Y}{X} \pm 180^\circ$$

$\overline{O'P'} = N(1 - e^2) + h$	(6 339 808,187 m) [6 339 723,236 m]
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$\overline{OP'} = R_{\psi_1} = \sqrt{X_1^2 + Z_1^2} = \sqrt{\overline{OO'}^2 + \overline{O'P'}^2 - 2 \overline{OO'} \overline{O'P'} \cos(180^\circ - \varphi)} =$ $= \sqrt{[N e^2 \cos \varphi]^2 + [N(1 - e^2) + h]^2 - 2[N e^2 \cos \varphi][N(1 - e^2) + h] \cos(180^\circ - \varphi)}$ <p style="color: red; margin: 0;">Law of Cosines</p> $\overline{OP'} = R_{\psi_1} = \frac{\overline{O'P'} \sin(180^\circ - \varphi)}{\sin \psi_1} = \frac{\overline{OO'} \sin(180^\circ - \varphi)}{\sin \beta_1} \quad \text{Law of Sines}$	<p style="color: green; margin: 0;">(6 375 071,733 m)</p> <p style="color: blue; margin: 0;">[6 374 836,828 m]</p>
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$a = \overline{OO'} + \overline{O'O''} + \overline{O'O'''} + \overline{O'''A}$	<p style="color: green; margin: 0;">(6 378 388,000 m)</p> <p style="color: blue; margin: 0;">[6 378 137,000 m]</p>
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$\overline{PP'} = h = R_{\psi_1} - R_{\psi} = \sqrt{\Delta_x^2 + \Delta_y^2}$	<p style="color: green; margin: 0;">(493,000 m)</p> <p style="color: blue; margin: 0;">[493,000 m]</p>
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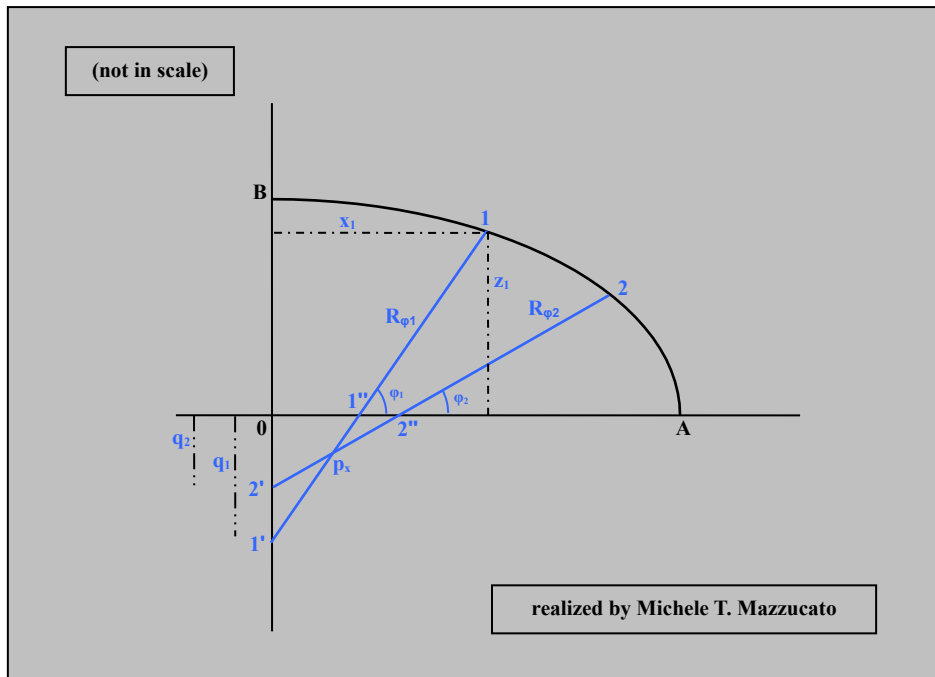
$180^\circ - \varphi$	<p style="color: green; margin: 0;">(155°)</p> <p style="color: blue; margin: 0;">[155°]</p>
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$\tan \psi = \frac{Z_0}{X_0}$ $\cos \psi = \frac{\overline{OO'}^2 + \overline{OP}^2 - \overline{O'P}^2}{2 \overline{OO'} \overline{OP}} = \frac{\overline{OO'}^2 + R_{\psi}^2 - R_{\varphi}^2}{2 \overline{OO'} R_{\psi}} =$ <p style="color: red; margin: 0;">Law of Cosines</p> $= \frac{[N \cos \varphi - N(1 - e^2) \cos \varphi]^2 + R_{\psi}^2 - [N(1 - e^2)]^2}{2[N \cos \varphi - N(1 - e^2) \cos \varphi] R_{\psi}}$ $\sin \psi = \frac{\overline{O'P} \sin(180^\circ - \varphi)}{\overline{OP}} = \frac{R_{\varphi} \sin(180^\circ - \varphi)}{R_{\psi}} \quad \text{Law of Sines}$	<p style="color: green; margin: 0;">(24,852290°)</p> <p style="color: blue; margin: 0;">[24,852913°]</p>
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$\tan \psi_1 = \frac{Z_1}{X_1}$ $\cos \psi_1 = \frac{\overline{OO'}^2 + \overline{OP'}^2 - \overline{O'P'}^2}{2 \overline{OO'} \overline{OP'}} = \frac{\overline{OO'}^2 + R_{\psi_1}^2 - (R_{\varphi} + h)^2}{2 \overline{OO'} R_{\psi_1}} =$ <p style="color: red; margin: 0;">Law of Cosines</p> $= \frac{[N \cos \varphi - N(1 - e^2) \cos \varphi]^2 + R_{\psi_1}^2 - [N(1 - e^2) + h]^2}{2[N \cos \varphi - N(1 - e^2) \cos \varphi] R_{\psi_1}}$ $\sin \psi_1 = \frac{\overline{O'P'} \sin(180^\circ - \varphi)}{\overline{OP'}} = \frac{(R_{\varphi} + h) \sin(180^\circ - \varphi)}{R_{\psi_1}} \quad \text{Law of Sines}$	<p style="color: green; margin: 0;">(24,852302°)</p> <p style="color: blue; margin: 0;">[24,852924°]</p>
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$\beta = 180^\circ - [\psi + (180^\circ - \varphi)]$ $\sin \beta = \frac{\overline{OO'} \sin(180^\circ - \varphi)}{\overline{OP}} = \frac{[N \cos \varphi - N(1 - e^2) \cos \varphi] \sin(180^\circ - \varphi)}{R_{\psi}} \quad \text{Law of Sines}$	<p style="color: green; margin: 0;">(0,147710°)</p> <p style="color: blue; margin: 0;">[0,147087°]</p>
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$\beta_1 = 180^\circ - [\psi_1 + (180^\circ - \varphi)]$ $\sin \beta_1 = \frac{\overline{OP'} \sin(180^\circ - \varphi)}{\overline{OP}} = \frac{[N \cos \varphi - N(1 - e^2) \cos \varphi] \sin(180^\circ - \varphi)}{R_{\psi_1}} \quad \text{Law of Sines}$	<p>(0,147698°) [0,147076°]</p>
$\psi + (180^\circ - \varphi) + \beta = 180^\circ$	<p>(180°) [180°]</p>
$\psi_1 + (180^\circ - \varphi) + \beta_1 = 180^\circ$	<p>(180°) [180°]</p>
$\alpha = \psi_1 - \psi \quad \sin \alpha = \frac{\overline{PP'} \sin \beta_1}{\overline{OP}} = \frac{h \sin \beta_1}{R_{\psi}} \quad \text{Law of Sines}$	<p>(0,000011423°) [0,000011375°]</p>
$\tan \varphi = \frac{Z_0}{R \varphi \cos \varphi} = \frac{Z_1}{R \varphi \cos \varphi + \Delta_x}$	<p>(25°) [25°]</p>



Note: equation of a straight line (equazione della retta)

equation of a straight line [implicit form] (equazione della retta in forma implicita)
 $ax + by + c = 0$

equation of a straight line [explicit form] (equazione della retta in forma esplicita)
 $y = mx + q$

where (con)

$m = -\frac{a}{b}$ and $m = \frac{y_2 - y_1}{x_2 - x_1}$ angular coefficient or gradient of the straight line (coefficiente angolare della retta)

$q = -\frac{c}{b}$ and $q = \frac{x_2 y_1 - x_1 y_2}{x_2 - x_1}$ ordinate at the origin of the straight line (ordinata all'origine della retta)

$d = \sqrt{(x_2 - x_1)^2 + (y_2 - y_1)^2}$ cartesian distance between two points (distanza tra due punti)

equation of the straight line from explicit to implicit form (equazione della retta da forma esplicita a forma implicita)
 $y = mx + q \Rightarrow -mx + y - q = 0$

$$\varphi_1 = 23^\circ$$

$$\lambda_1 = 0^\circ$$

$$m_1 = \tan \varphi_1 = 0,424474816$$

$$q_1 = N_1 e^2 \sin \varphi_1 = -16763,076 \text{ m}$$

$$x_1 = N_1 \cos \varphi_1 \cos \lambda_1 = 5874352,472 \text{ m}$$

$$y_1 = m_1 x_1 + q_1 \quad y_1 = Z_1 = R_{\varphi_1} \sin \varphi_1 = N_1 (1 - e^2) \sin \varphi_1 = 2476751,610 \text{ m}$$

point 1'' coordinates on the X axis (coordinate punto 1'' sull'asse delle X)

$$x_{1''} = \overline{O1''} = N_1 e^2 \cos \varphi_1 = N_1 \cos \varphi_1 \cos \lambda_1 - N_1 (1 - e^2) \cos \varphi_1 = 39491,333 \text{ m}$$

$$y_{1''} = 0 \text{ m}$$

$$R_{\varphi_1} = d_{11''} = \sqrt{(x_1 - x_{1''})^2 + (y_1 - y_{1''})^2} = 6338761,949 \text{ m}$$

$$q_1 = \frac{x_1 y_1'' - x_1'' y_1}{x_1 - x_1''} = -16763,076 \text{ m}$$

$$y_1 = m_1 x_1 + q_1 \Rightarrow -m_1 x_1 + y_1 - q_1 = 0$$

$$\varphi_2 = 12^\circ$$

$$\lambda_2 = 0^\circ$$

$$m_2 = \tan \varphi_2 = 0,212556562$$

$$q_2 = N_2 e^2 \sin \varphi_2 = -8916,507 \text{ m}$$

$$x_2 = N_2 \cos \varphi_2 \cos \lambda_2 = 6239911,652 \text{ m}$$

$$y_2 = m_2 x_2 + q_2 \quad y_2 = Z_2 = R_{\varphi_2} \sin \varphi_2 = N_2 (1 - e^2) \sin \varphi_2 = 1317417,659 \text{ m}$$

point 2'' coordinates on the X axis (coordinate punto 2'' sull'asse delle X)

$$x_{2''} = \overline{02''} = N_2 e^2 \cos \varphi_2 = N_2 \cos \varphi_2 \cos \lambda_2 - N_2 (1 - e^2) \cos \varphi_2 = 41948,867 \text{ m}$$

$$y_{2''} = 0 \text{ m}$$

$$R_{\varphi_2} = d_{22''} = \sqrt{(x_2 - x_{2''})^2 + (y_2 - y_{2''})^2} = 6336428,961 \text{ m}$$

$$q_2 = \frac{x_2 y_{2''} - x_{2''} y_2}{x_2 - x_{2''}} = -8916,507 \text{ m}$$

$$y_2 = m_2 x_2 + q_2 \Rightarrow -m_2 x_2 + y_2 - q_2 = 0$$

Note: Cramer's rule for linear systems of 2 equations in 2 variables
(Metodo di Cramer per sistemi lineari di 2 equazioni in 2 incognite)

$$\begin{cases} a_1 x + b_1 y = c_1 \\ a_2 x + b_2 y = c_2 \end{cases}$$

matrix of coefficients (matrice dei coefficienti)

$$\begin{bmatrix} a_1 & b_1 \\ a_2 & b_2 \end{bmatrix}$$

determinant of the matrix 2x2 (determinante della matrice 2x2)

$$D = (a_1 \cdot b_2) - (a_2 \cdot b_1)$$

if $D = 0$ indeterminate or impossible system, do not proceed (se $D=0$ sistema indeterminato o impossibile, non si procedere)
if $D \neq 0$ system determined, proceed (se $D \neq 0$ sistema determinato, si procede)

determinant of the variable x (determinante dell'incognita x)

$$D_x = \begin{bmatrix} c_1 & b_1 \\ c_2 & b_2 \end{bmatrix} = (c_1 \cdot b_2) - (c_2 \cdot b_1)$$

determinant of the variable y (determinante dell'incognita y)

$$D_y = \begin{bmatrix} a_1 & c_1 \\ a_2 & c_2 \end{bmatrix} = (a_1 \cdot c_2) - (a_2 \cdot c_1)$$

2x2 system solutions (soluzioni del sistema 2x2)

$$x = \frac{D_x}{D} \quad y = \frac{D_y}{D}$$

[from Gabriel Cramer (1704-1752) in *Introduction a l'analyse des courbes algebriques* (1750) in which he introduces Cramer's rule for solving a system of linear equations. Colin Maclaurin (1698-1746) in *Treatise of algebra* (1748) also dealt with it and provided its proof for linear systems with two and three unknowns.]

[da Gabriel Cramer (1704-1752) in *Introduction a l'analyse des courbes algebriques* (1750) in cui introduce la *regola di Cramer* per la risoluzione di un sistema di equazioni lineari. Anche Colin Maclaurin (1698-1746) in *Treatise of algebra* (1748) ne trattò e ne fornì la dimostrazione per sistemi lineari con due e tre incognite.]

point of intersection between two straight lines (*elimination of variables method*)
(punto di intersezione tra due rette, *metodo di sostituzione*)

$$\begin{cases} -m_1 x_1 + y_1 = q_1 \\ -m_2 x_2 + y_2 = q_2 \end{cases}$$

$$\begin{cases} -0,424474816x_1 + y_1 = -16763,076 \\ -0,212556562x_2 + y_2 = -8916,507 \end{cases}$$

$$\begin{cases} y = 0,424474816x - 16763,076 \\ -0,212556562x + y = -8916,507 \end{cases}$$

$$\begin{cases} y = 0,424474816x - 16763,076 \\ -0,212556562x + (0,424474816x - 16763,076) = -8916,507 \end{cases}$$

$$\begin{cases} y = 0,424474816x - 16763,076 \\ 0,211918254x - 16763,076 = -8916,507 \end{cases}$$

$$\begin{cases} y = 0,424474816x - 16763,076 \\ 0,211918254x = 7846,569 \end{cases}$$

$$\begin{cases} y = 0,424474816x - 16763,076 \\ x = \frac{7846,569}{0,211918254} = 37026,395 \end{cases}$$

$$\begin{cases} y_{p_x} = 0,424474816 \cdot 37026,395 - 16763,076 = -1046,304 \\ x_{p_x} = 37026,396 \end{cases}$$

point of intersection between two straight lines (*Cramer's rule*) for verification
(punto di intersezione tra due rette, *metodo di Cramer per verifica*)

$$\begin{cases} -m_1 x_1 + y_1 = q_1 \\ -m_2 x_2 + y_2 = q_2 \end{cases}$$

$$\begin{cases} -0,424474816x_1 + y_1 = -16763,076 \\ -0,212556562x_2 + y_2 = -8916,507 \end{cases}$$

$$\begin{bmatrix} -m_1 & 1 \\ -m_2 & 1 \end{bmatrix}$$

determinant of the matrix 2x2 (determinante della matrice 2x2)

$$D = (-m_1 \cdot 1) - (-m_2 \cdot 1) = -0,211918254$$

if $D \neq 0$ system determined, proceed (se $D \neq 0$ sistema determinato, si procede)

determinant of the variable x (determinante dell'incognita x)

$$D_x = \begin{bmatrix} -q_1 & 1 \\ -q_2 & 1 \end{bmatrix} = (-q_1 \cdot 1) - (-q_2 \cdot 1) = -7846,569$$

determinant of the variable y (determinante dell'incognita y)

$$D_y = \begin{bmatrix} -m_1 & -q_1 \\ -m_2 & -q_2 \end{bmatrix} = (-m_1 \cdot -q_2) - (-m_2 \cdot -q_1) = 221,731$$

2x2 system solutions (soluzioni del sistema 2x2)

$$y_{p_x} = \frac{D_y}{D} = -1046,304 \quad x_{p_x} = \frac{D_x}{D} = 37026,395$$